



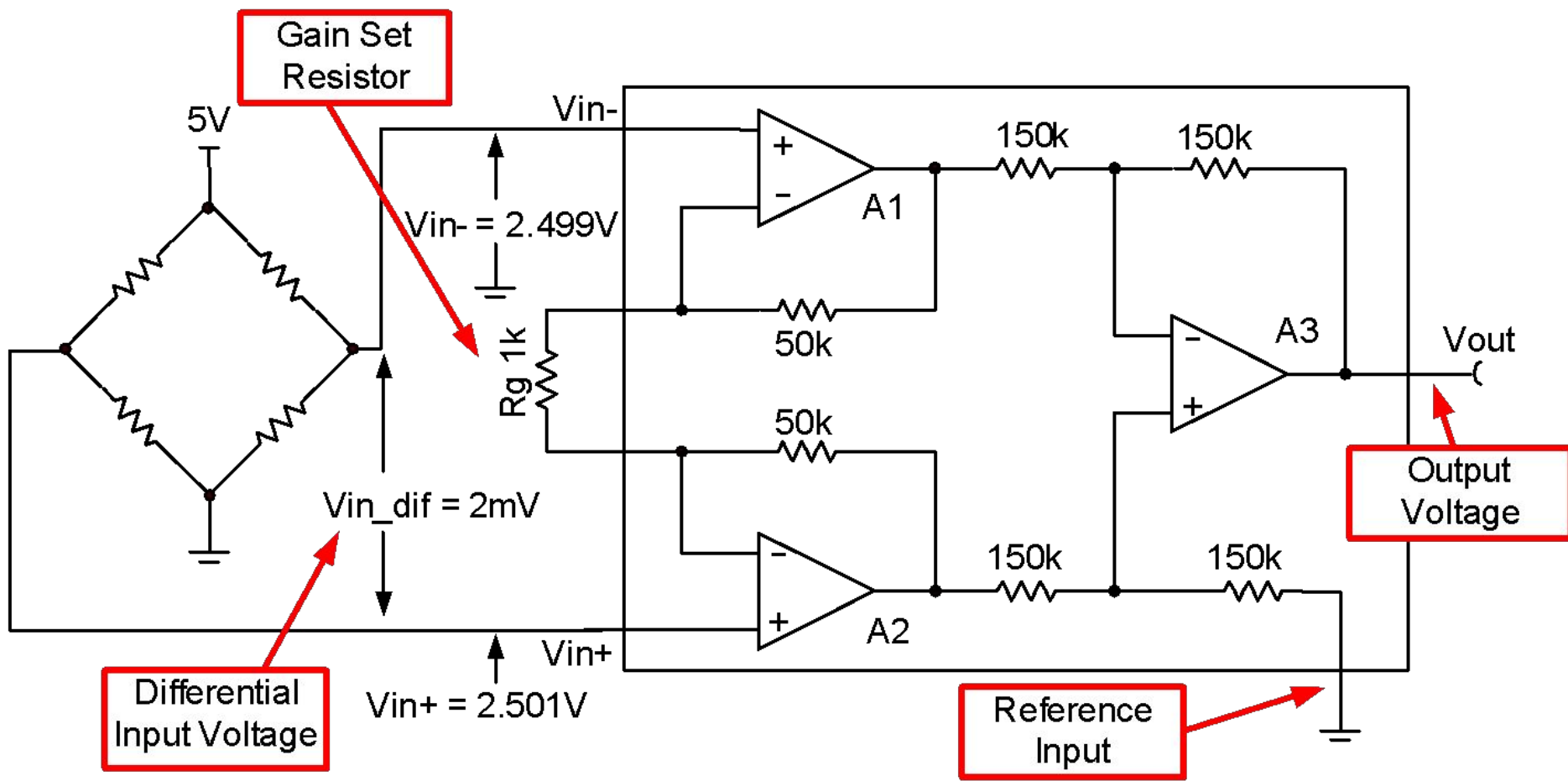
Instrumentation Amplifier Noise Analysis



SHORT RANGE OF BANDWIDTH

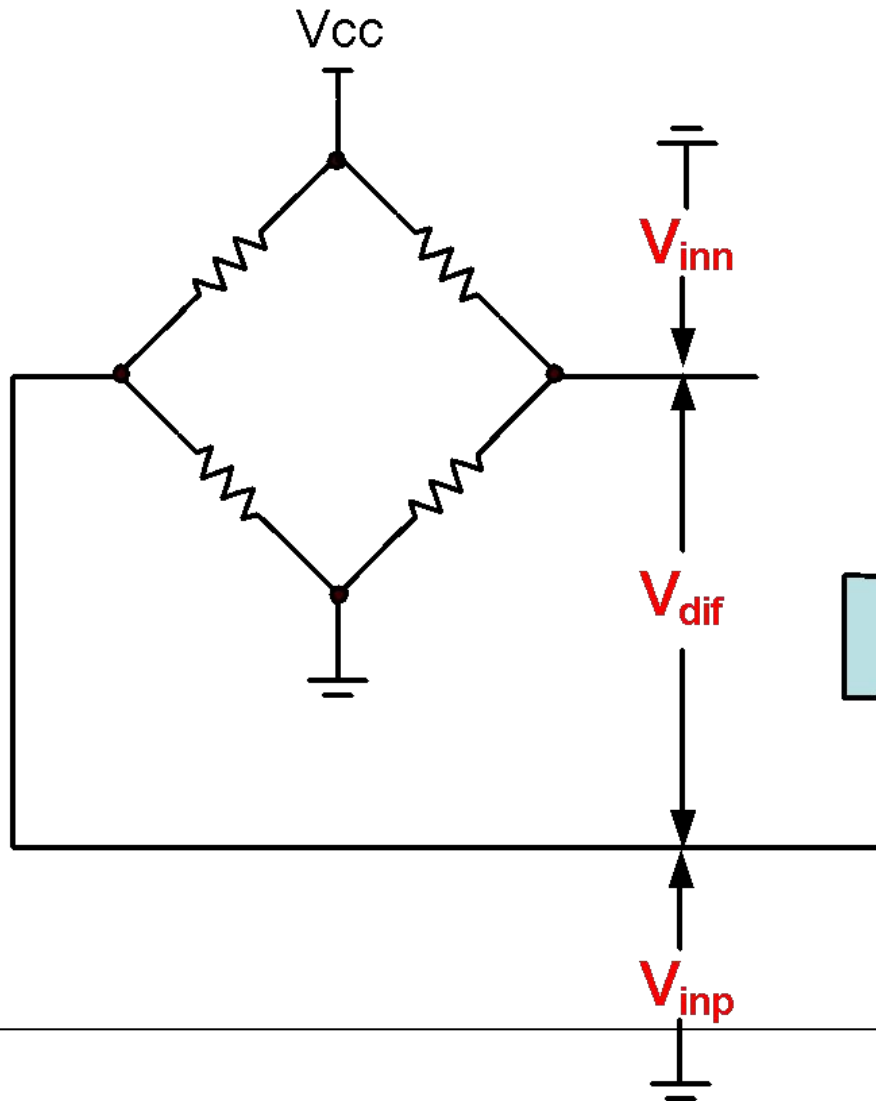


Three Stage IA

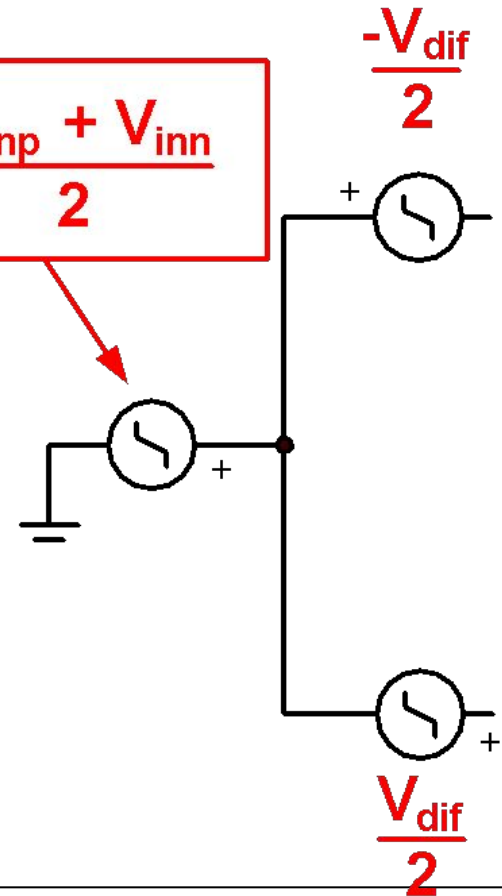
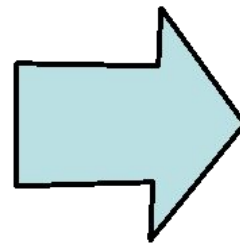




Real World Input to Mathematical Model

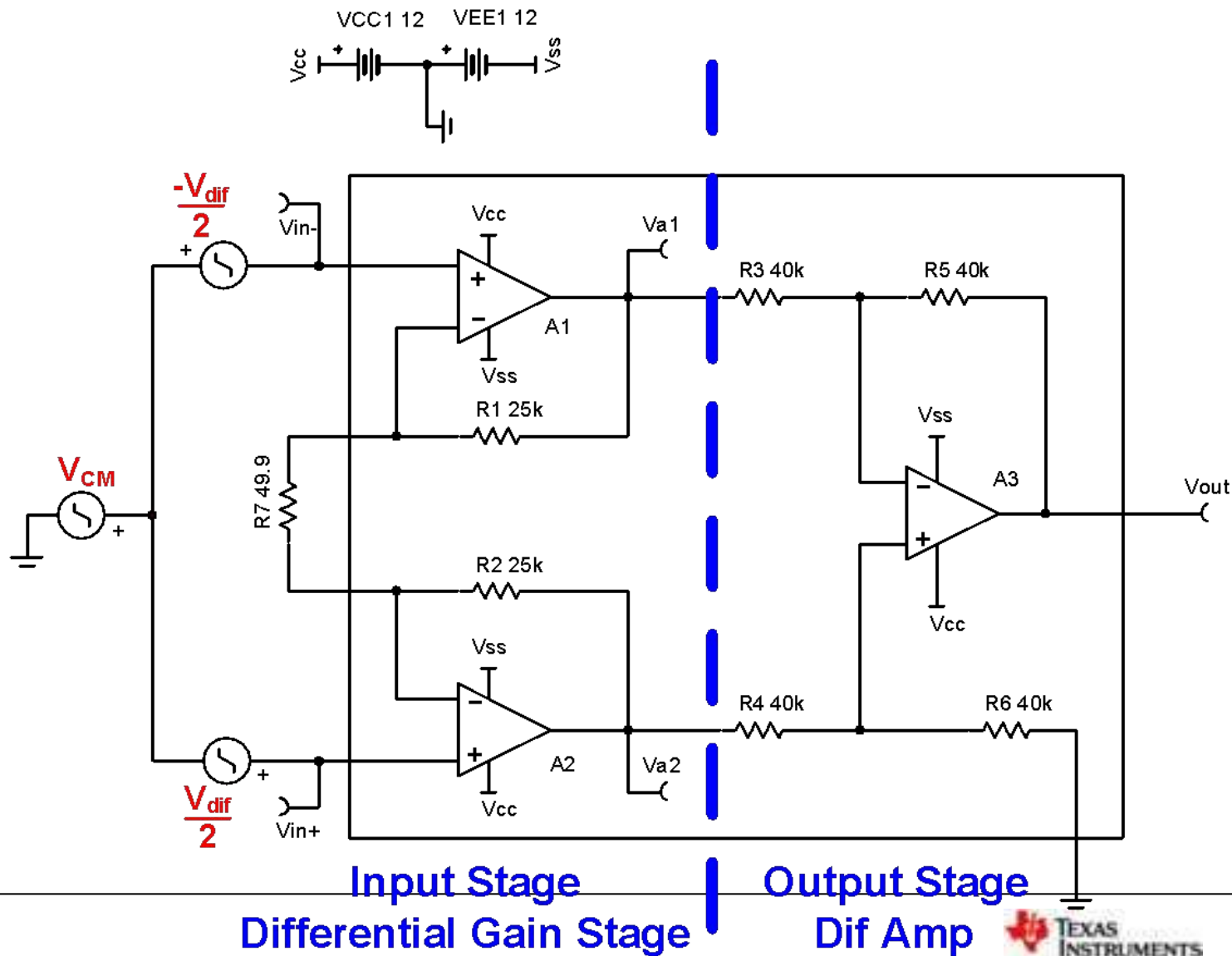


$$V_{cm} = \frac{V_{inp} + V_{inn}}{2}$$



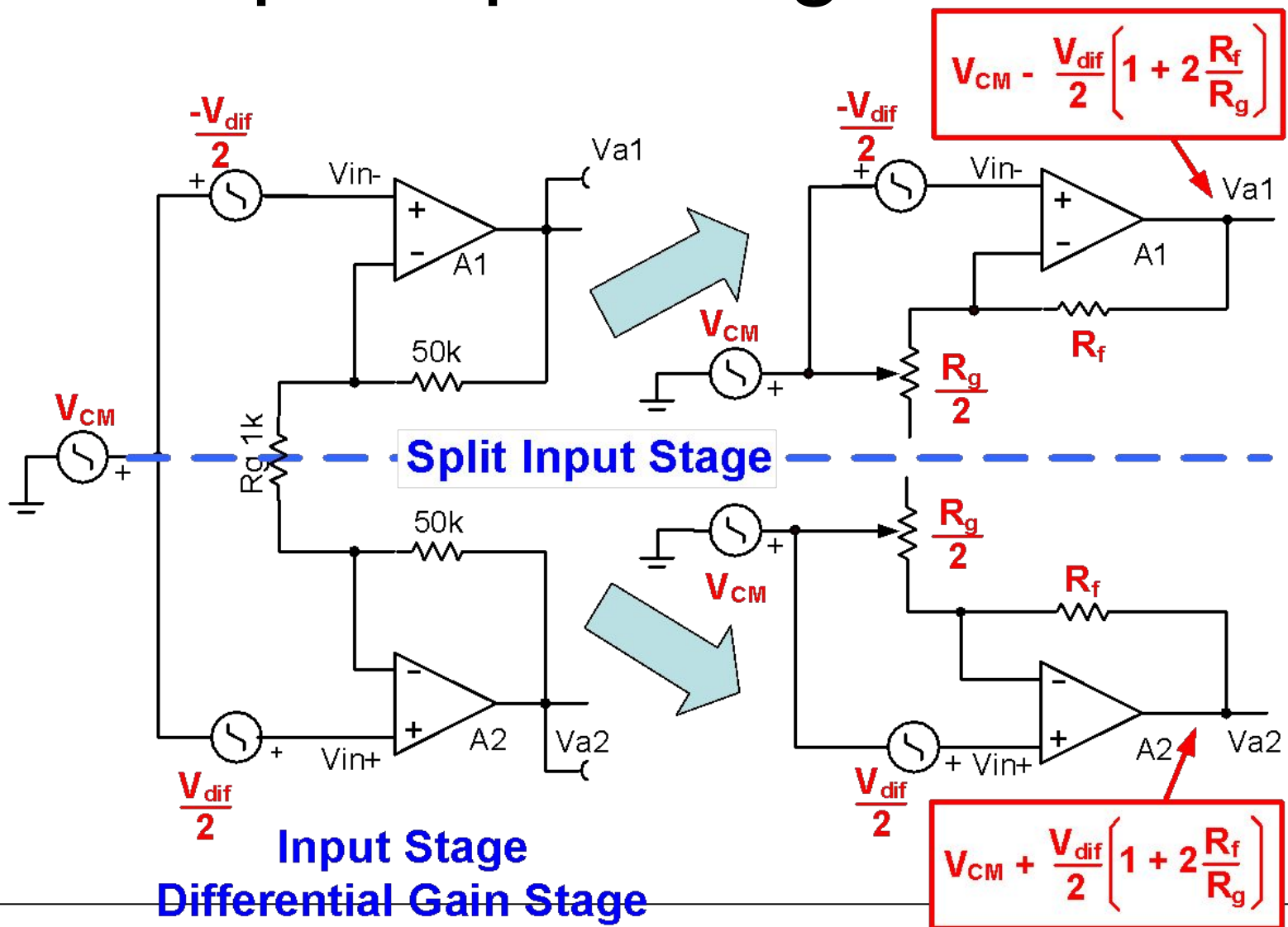


Analyze the Input and Output Separately



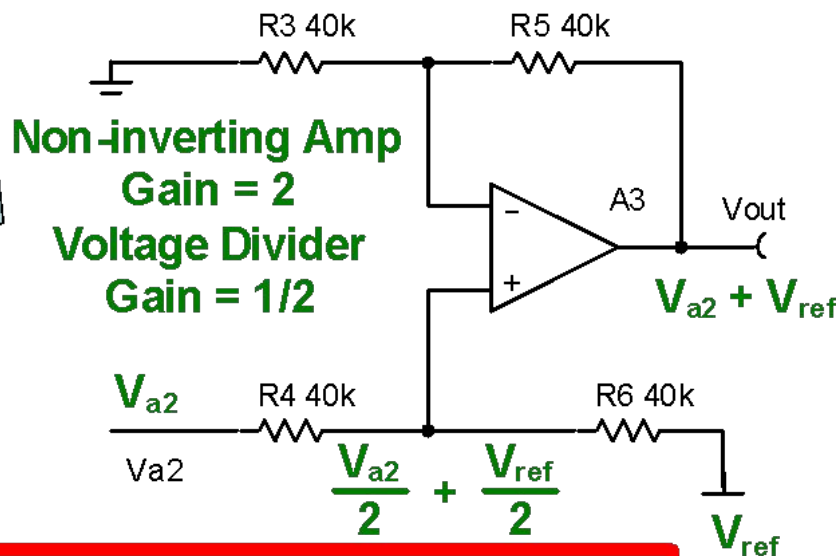
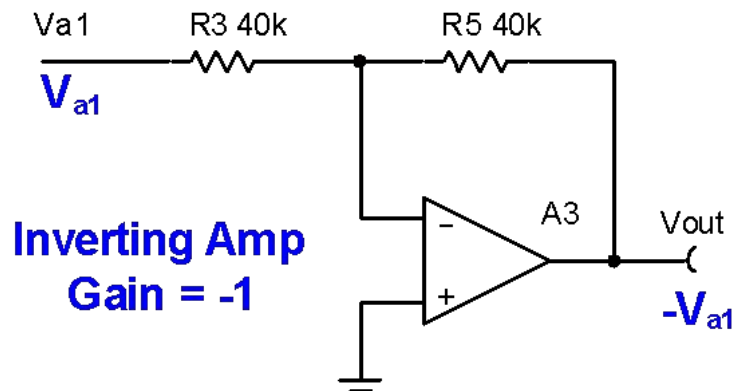
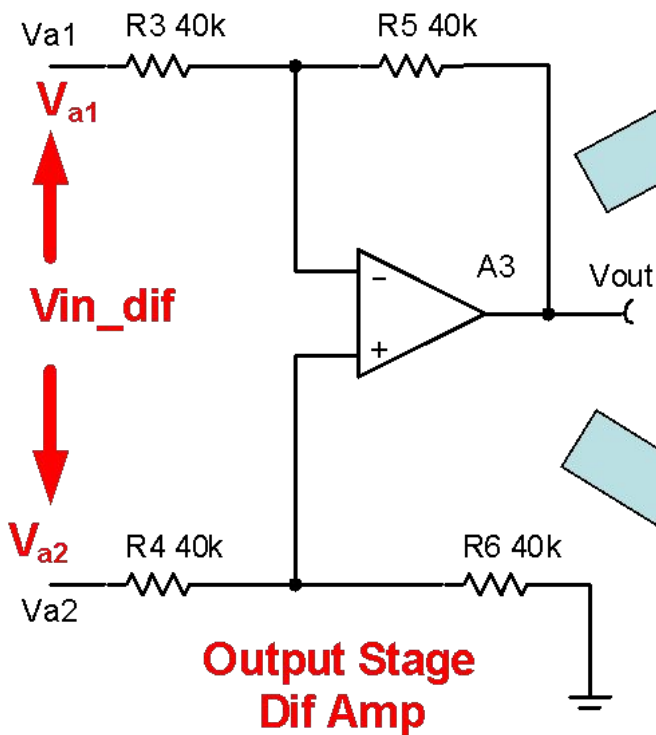


Split Input Stage in Half





Use Superposition on Output Amp



Find Vout Through Superposition

$$V_{out} = V_{a2} - V_{a1} + V_{ref}$$



Gain For Three Amp IA

$$V_{a1} = V_{cm} - \frac{V_{dif}}{2} \cdot \left(1 + 2 \frac{R_f}{R_g} \right) \quad \text{[1] Input Stage Top Half}$$

$$V_{a2} = V_{cm} + \frac{V_{dif}}{2} \cdot \left(1 + 2 \frac{R_f}{R_g} \right) \quad \text{[2] Input Stage Bottom Half}$$

$$V_{out} = V_{a2} - V_{a1} + V_{ref} \quad \text{[3] Output Stage}$$

$$V_{out} = \left[V_{cm} + \frac{V_{dif}}{2} \cdot \left(1 + 2 \frac{R_f}{R_g} \right) \right] - \left[V_{cm} - \frac{V_{dif}}{2} \cdot \left(1 + 2 \frac{R_f}{R_g} \right) \right] + V_{ref} \quad \text{Substitute [1] and [2] into [3]}$$

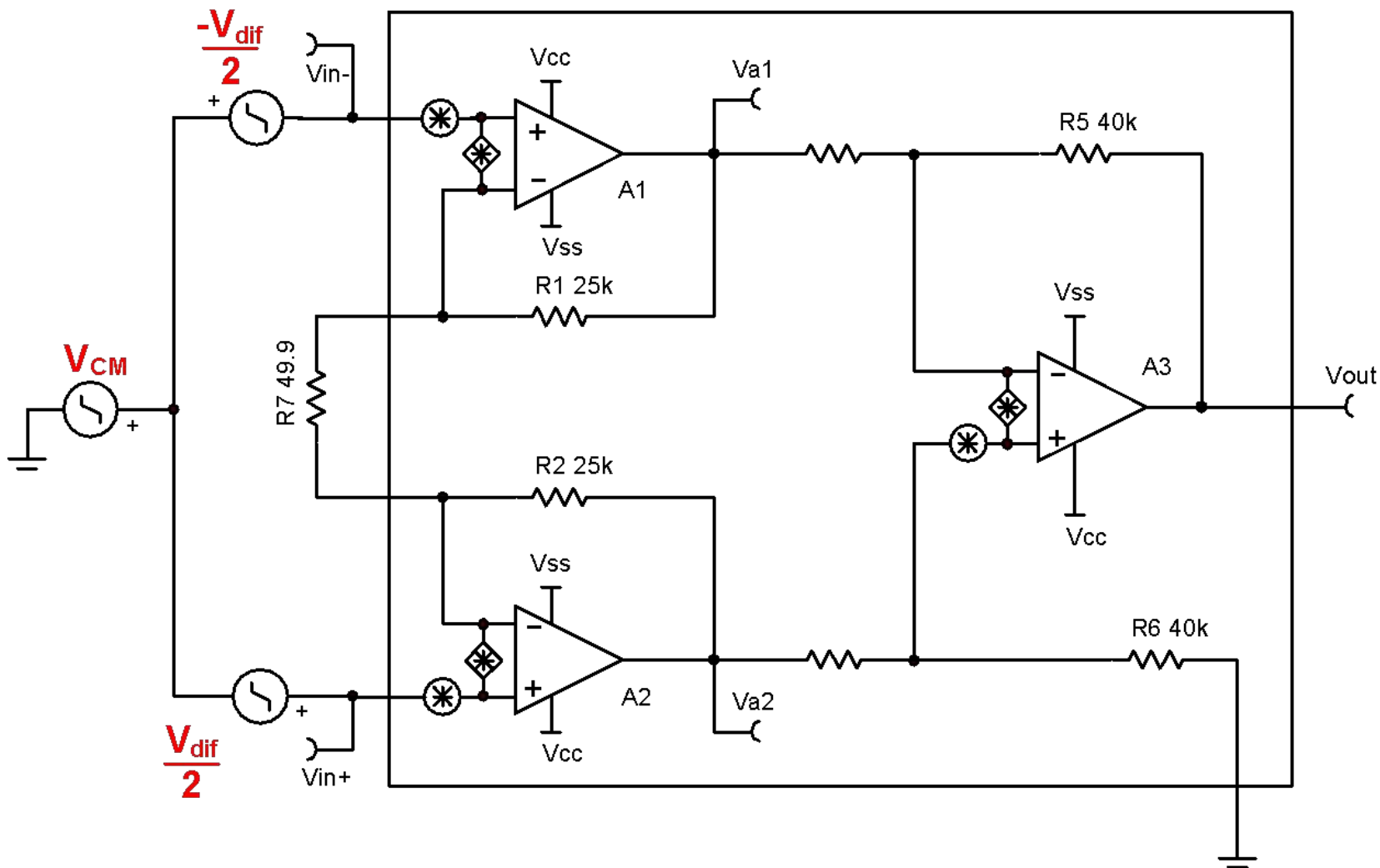
$$V_{out} = V_{dif} \left(1 + 2 \frac{R_f}{R_g} \right) + V_{ref} \quad \text{[4] Simplify}$$



MESSAGE FROM THE BOARD

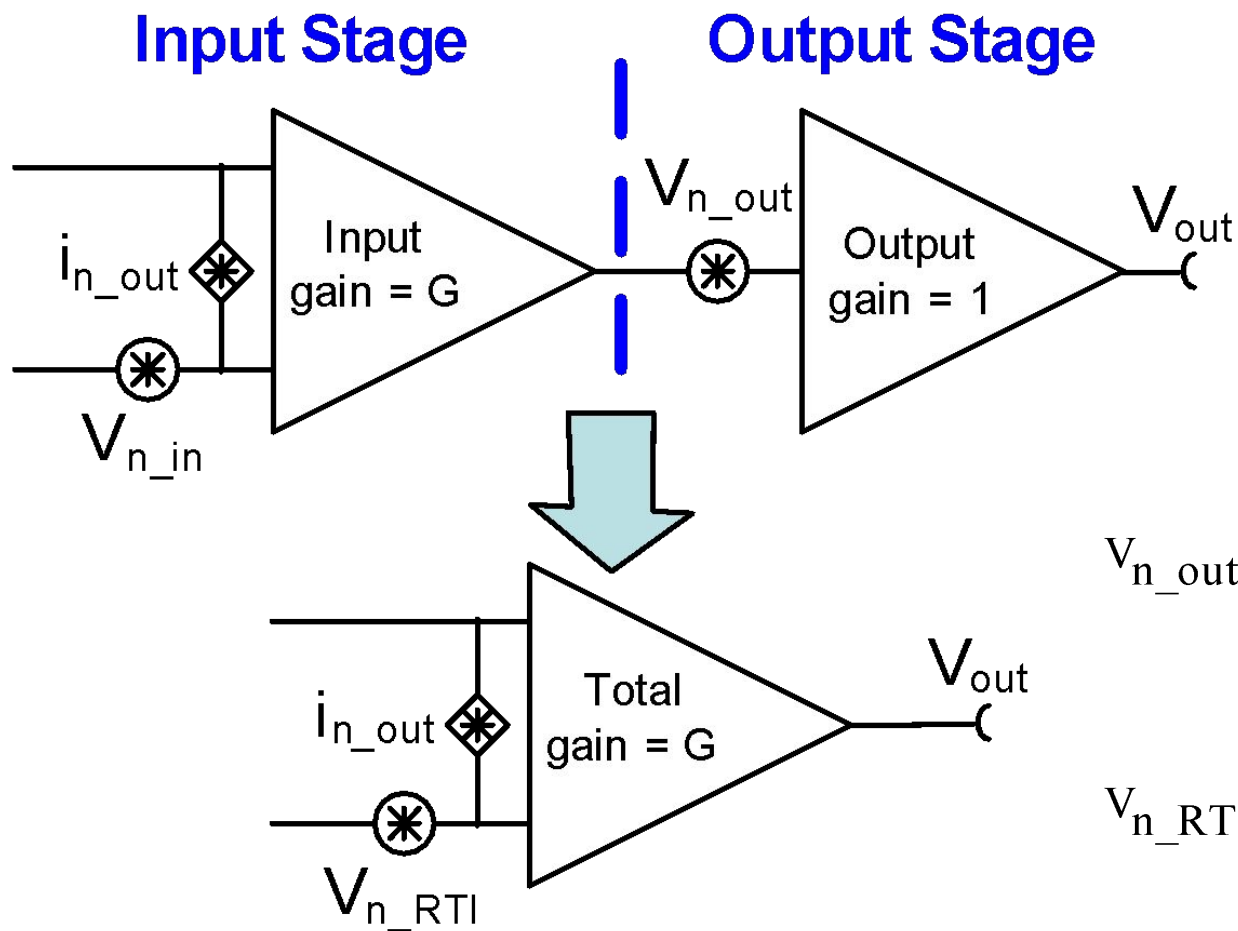


Complex Noise Model





The Complex Model is Simplified

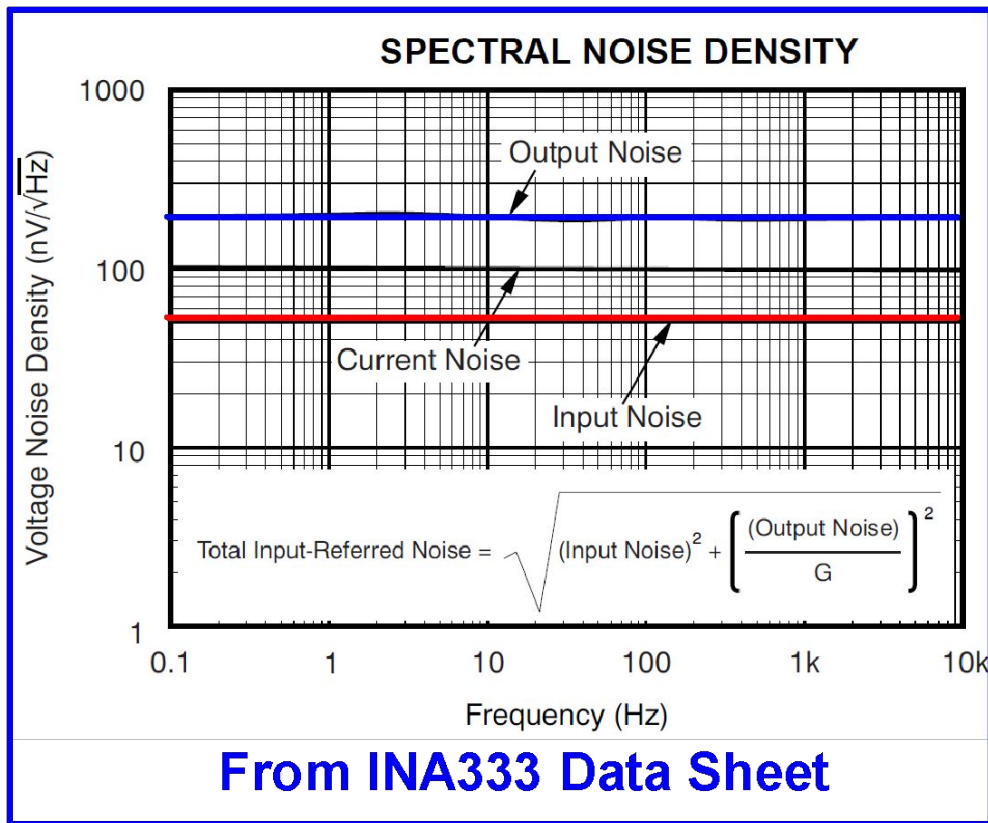


$$V_{n_out} = \sqrt{(V_{n_out})^2 + (V_{n_in} \cdot G)^2}$$

$$V_{n_RTI} = \sqrt{\left(\frac{V_{n_out}}{G}\right)^2 + (V_{n_in})^2}$$



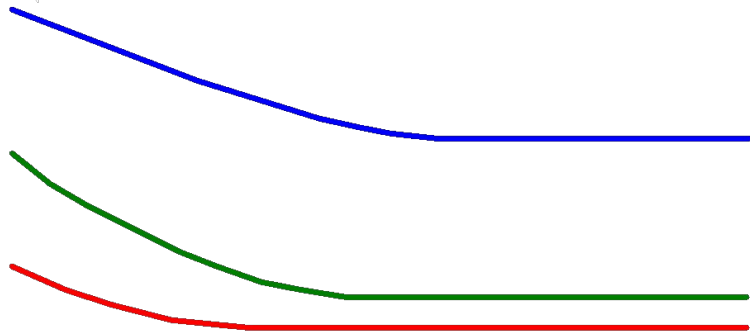
The Input amplifier dominates at High Gain



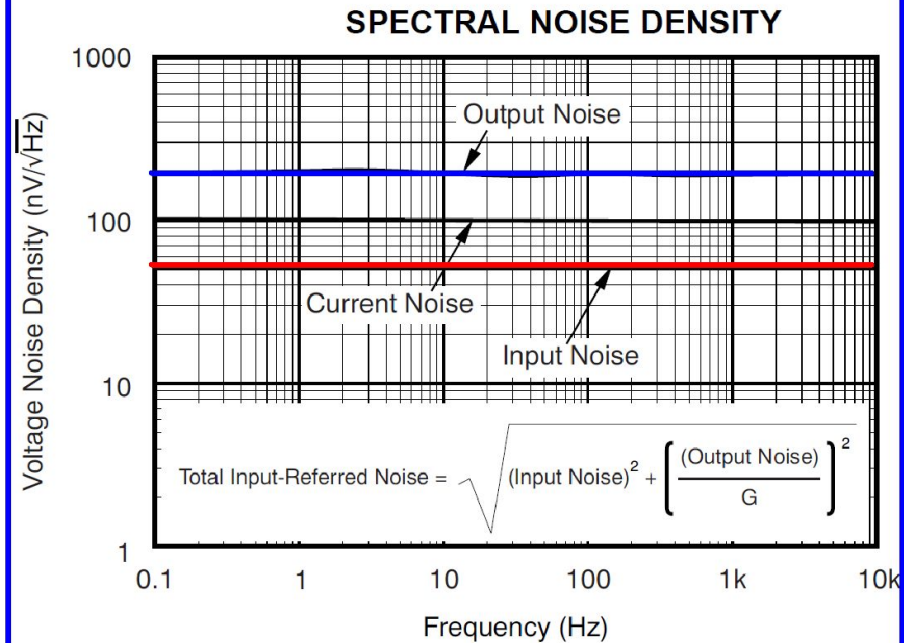
G	Total Input-Referr ed Noise (nV/rtHz)	Total Output Noise (nV/rtHz)
1	206.2	206.2
2	111.8	223.6
5	64	320
10	53.9	539
100	50	5000
1000	50	50,000



Two Ways to represent INA Spectral Density



From INA128 Data Sheet



From INA333 Data Sheet

G	Input-Referred Noise (nV/rtHz)
1	110
10	12
100	8
1000	8

Taken directly from the graph

G	Input-Referred Noise (nV/rtHz)
1	206.2
10	53.9
100	50
1000	50

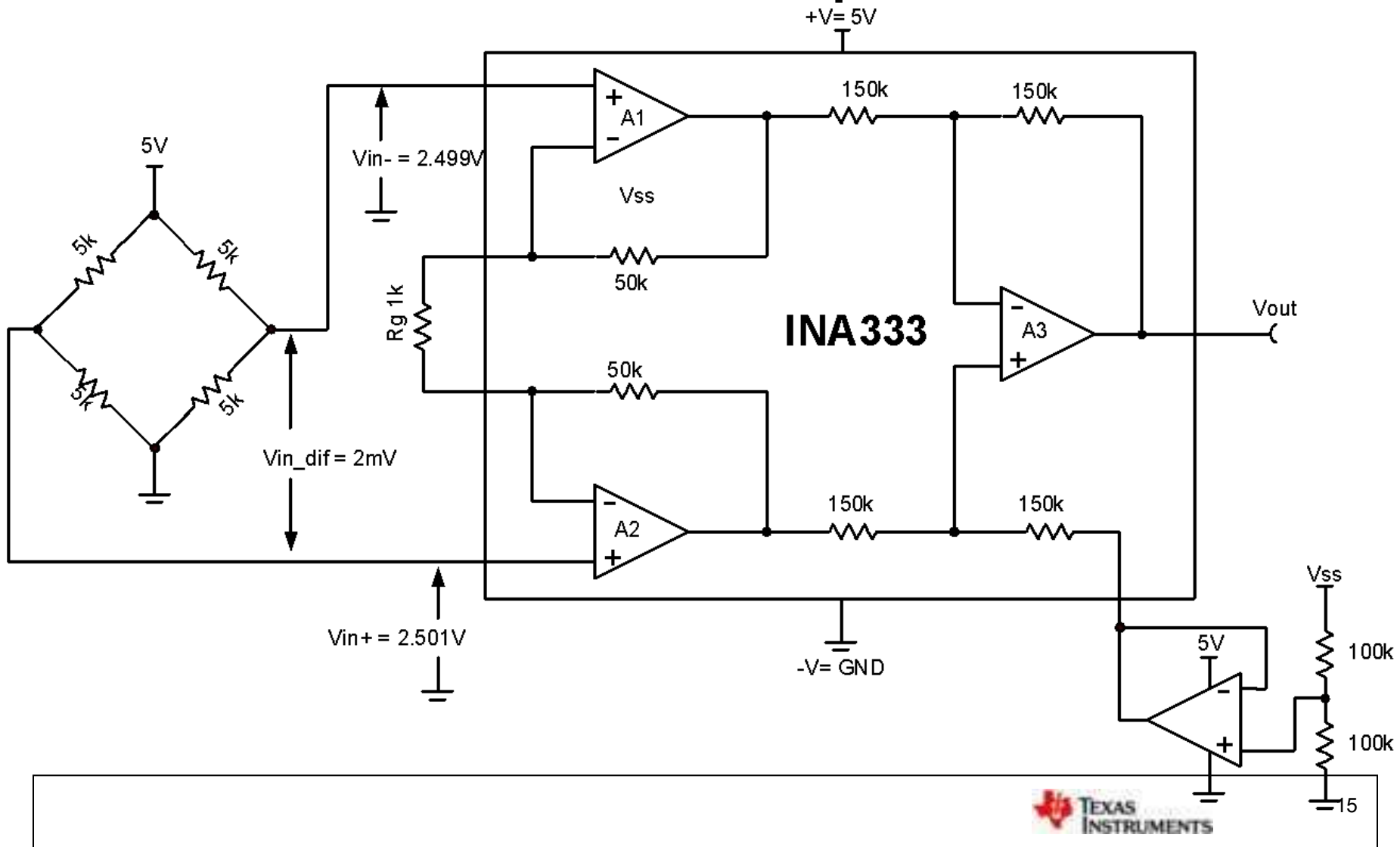
Calculated using graphs and formula



Hand Analysis of a Handwritten Signature

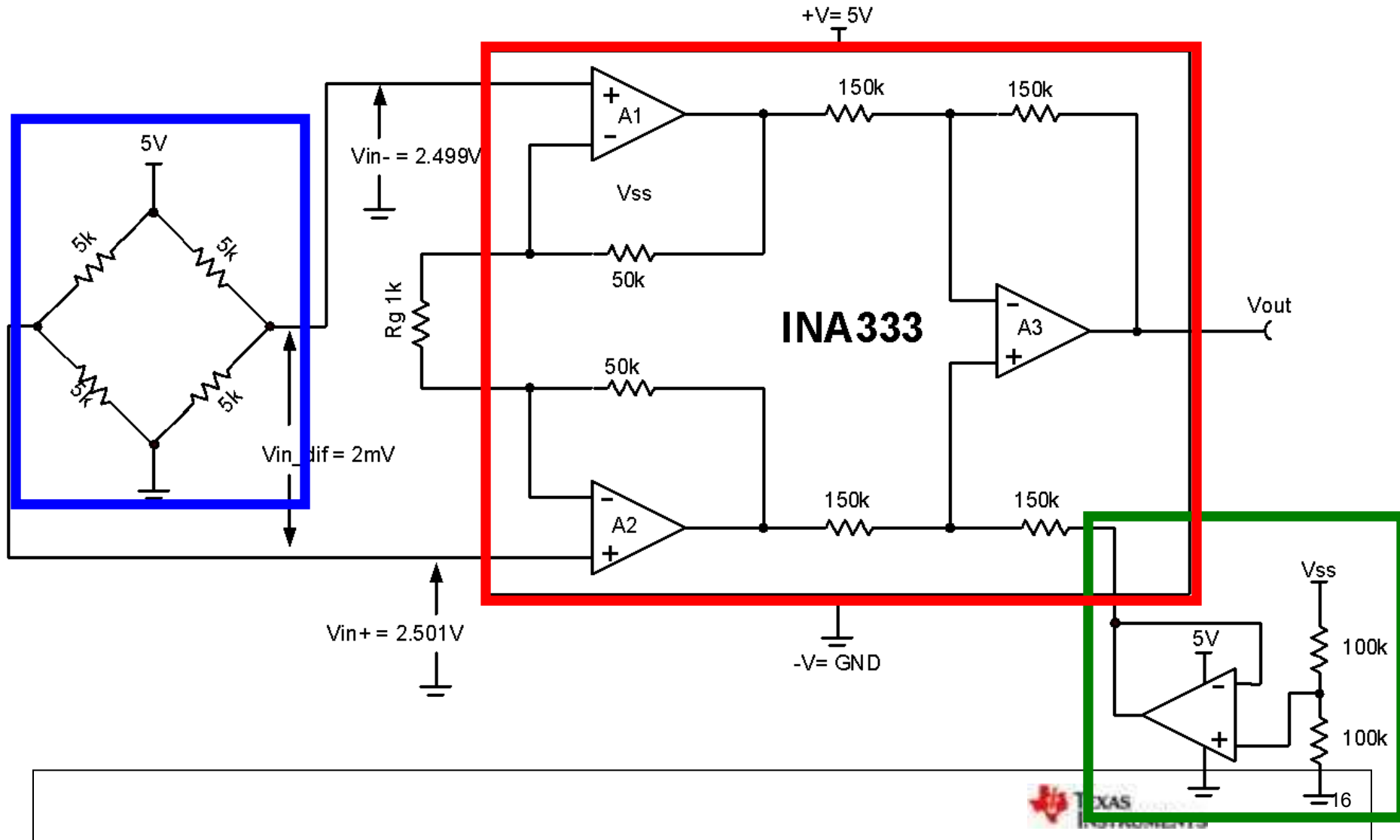


Find the total RMS Noise Voltage at the Output



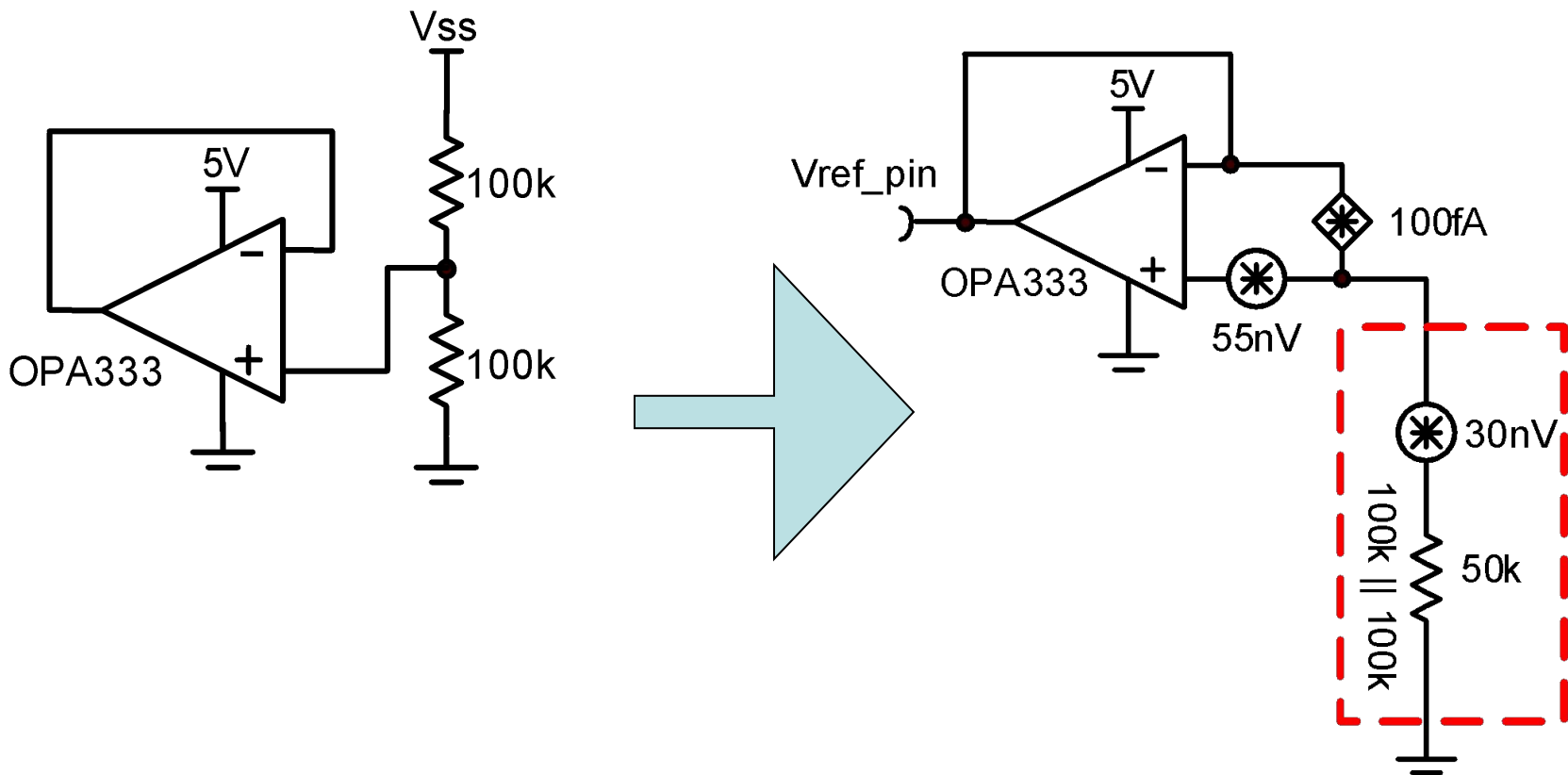


Look at Noise Sources: Bridge, INA333, Reference Buffer



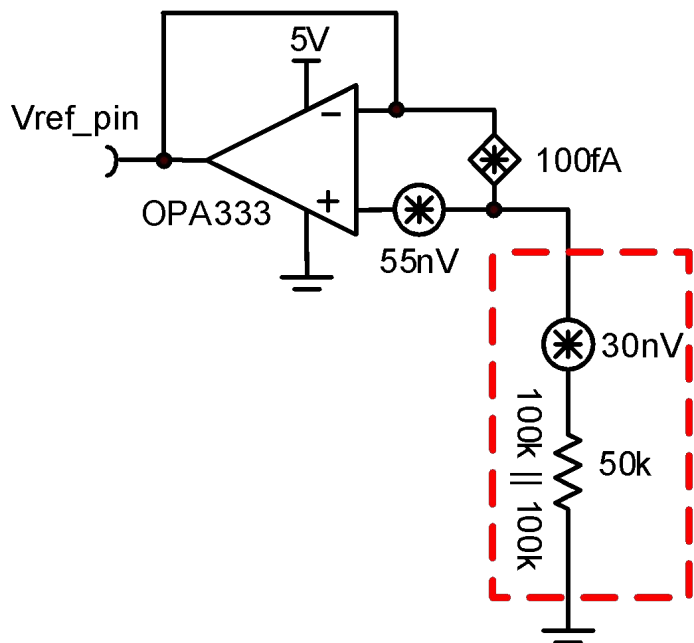


Noise Equivalent Model for Reference Pin Buffer





Reference buffer



$$k_n = 1.38 \cdot 10^{-23} \quad \text{Boltzmann's constant}$$

$$T_k = 273 + 25 \quad \text{Temperature in Kelvin}$$

$$R_{eq} = 50k\Omega \quad \text{Input resistance (parallel combination of voltage divider)}$$

$$e_{n_r} = \sqrt{4k_n \cdot T_n \cdot R_{eq}} = 28.7 \frac{\text{nV}}{\sqrt{\text{Hz}}} \quad \text{Thermal Noise from input resistor}$$

$$i_n = 100\text{fA} \quad \text{Current noise from OPA333}$$

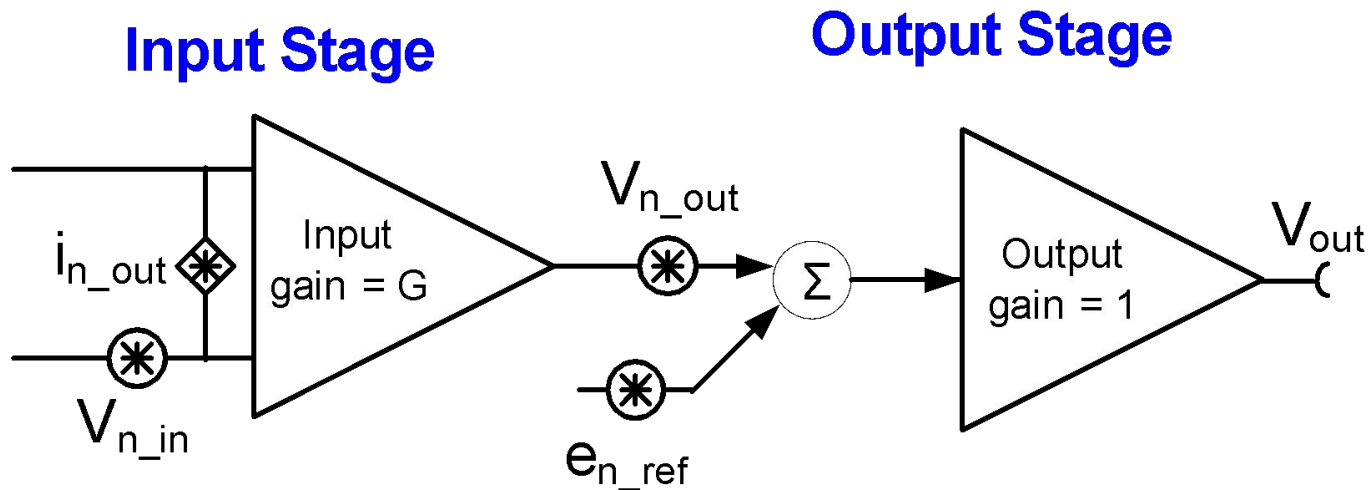
$$e_{n_i} = i_n \cdot R_{eq} = 5 \frac{\text{nV}}{\sqrt{\text{Hz}}} \quad \text{Voltage Noise from current noise}$$

$$e_{n_{opa}} = 55 \frac{\text{nV}}{\sqrt{\text{Hz}}} \quad \text{Voltage noise from OPA333}$$

$$e_{n_{ref}} = \sqrt{e_{n_{opa}}^2 + e_{n_r}^2 + e_{n_i}^2} = 62.2 \frac{\text{nV}}{\sqrt{\text{Hz}}} \quad \text{Total rms noise from reference driver circuit}$$



The reference voltage directly adds to the output noise

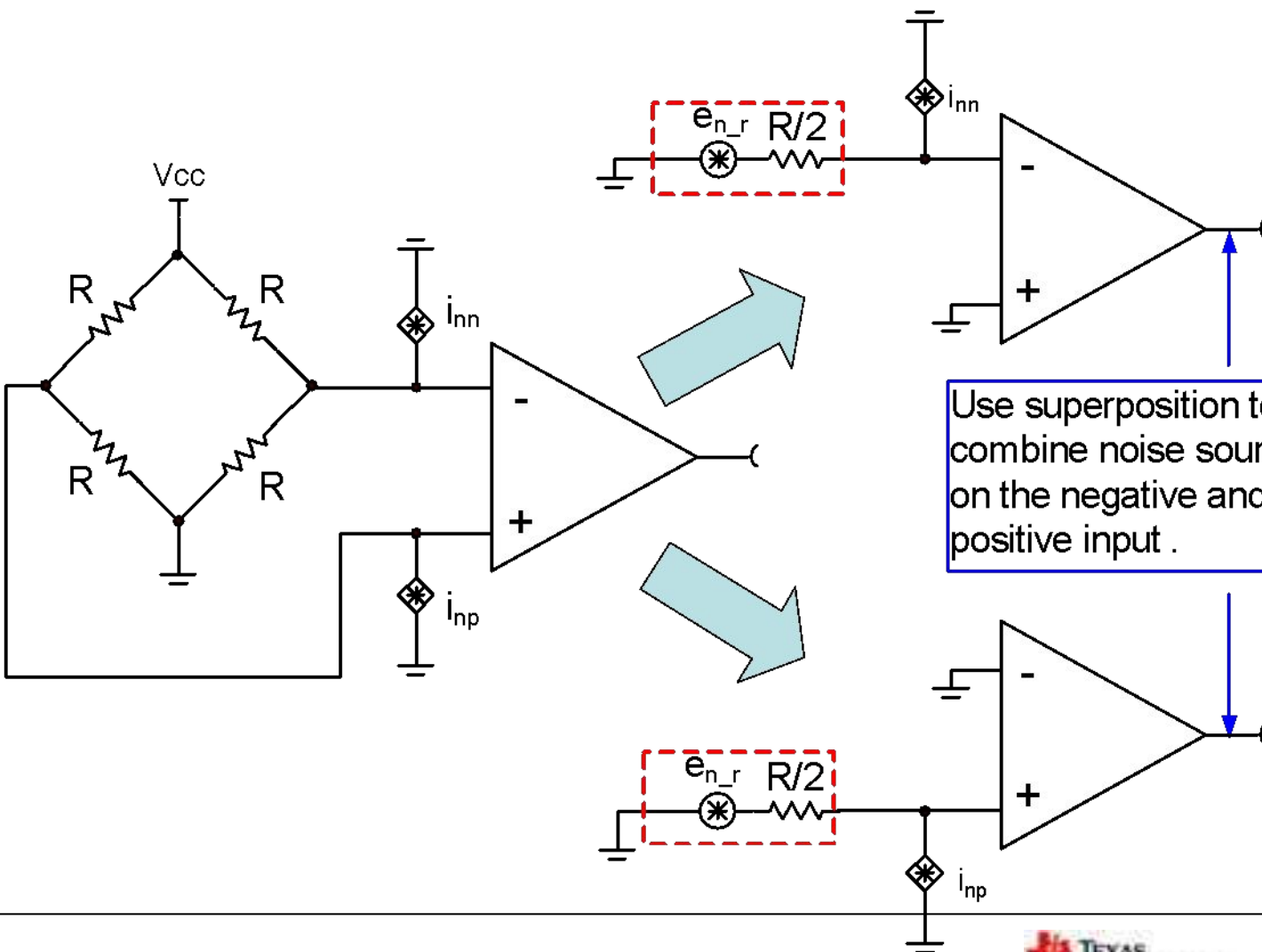


$$e_{n_ref} := 62.2 \cdot 10^{-9} \quad V_{n_out} := 200 \cdot 10^{-9}$$

$$\text{Output_Stage_Noise} := \sqrt{e_{n_ref}^2 + V_{n_out}^2} = 209.449 \times 10^{-9}$$

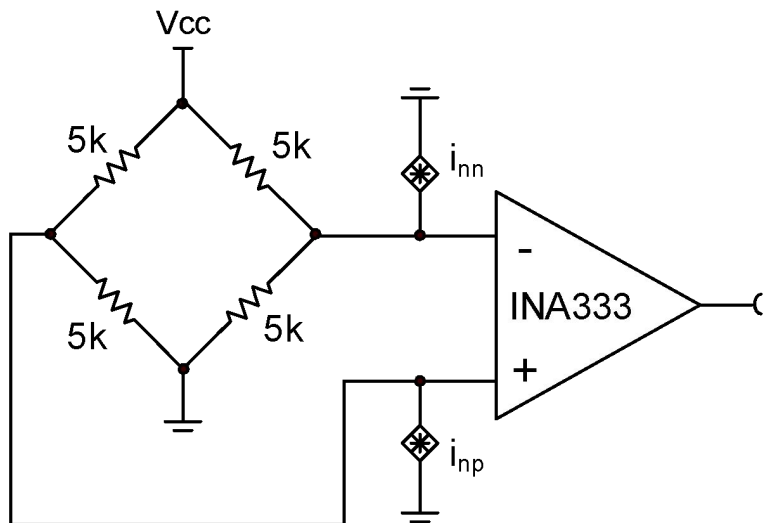


The bridge generates: thermal noise, $i_n \times R_{\text{bridge}}$





Noise From Bridge / Current Sources



$$i_{nn} \cdot \frac{R}{2} \quad \text{Voltage noise from current noise}$$

$$e_{n_rb} = \sqrt{4k_n \cdot T_n \cdot \frac{R}{2}} \quad \text{Resistor Noise}$$

Use superposition to add the noise from the input resistance and both current noise sources

$$e_{in_i} = \sqrt{\left(i_{nn} \cdot \frac{R}{2}\right)^2 + (e_{n_rb})^2 + \left(i_{np} \cdot \frac{R}{2}\right)^2 + (e_{n_rb})^2}$$

$$\text{Assume } |i_{nn}| = |i_{np}|$$

Note that these sources are uncorrelated

$$e_{in_i} = \sqrt{2\left(i_n \cdot \frac{R}{2}\right)^2 + 2(e_{n_rb})^2} \quad \text{Total Noise from input resistors and current source}$$

For this example ($R=5k\Omega$, $i_n = 100fA/\sqrt{Hz}$)

$$e_{n_rb} = 6.4 \frac{nV}{\sqrt{Hz}} \quad \text{Resistor noise}$$

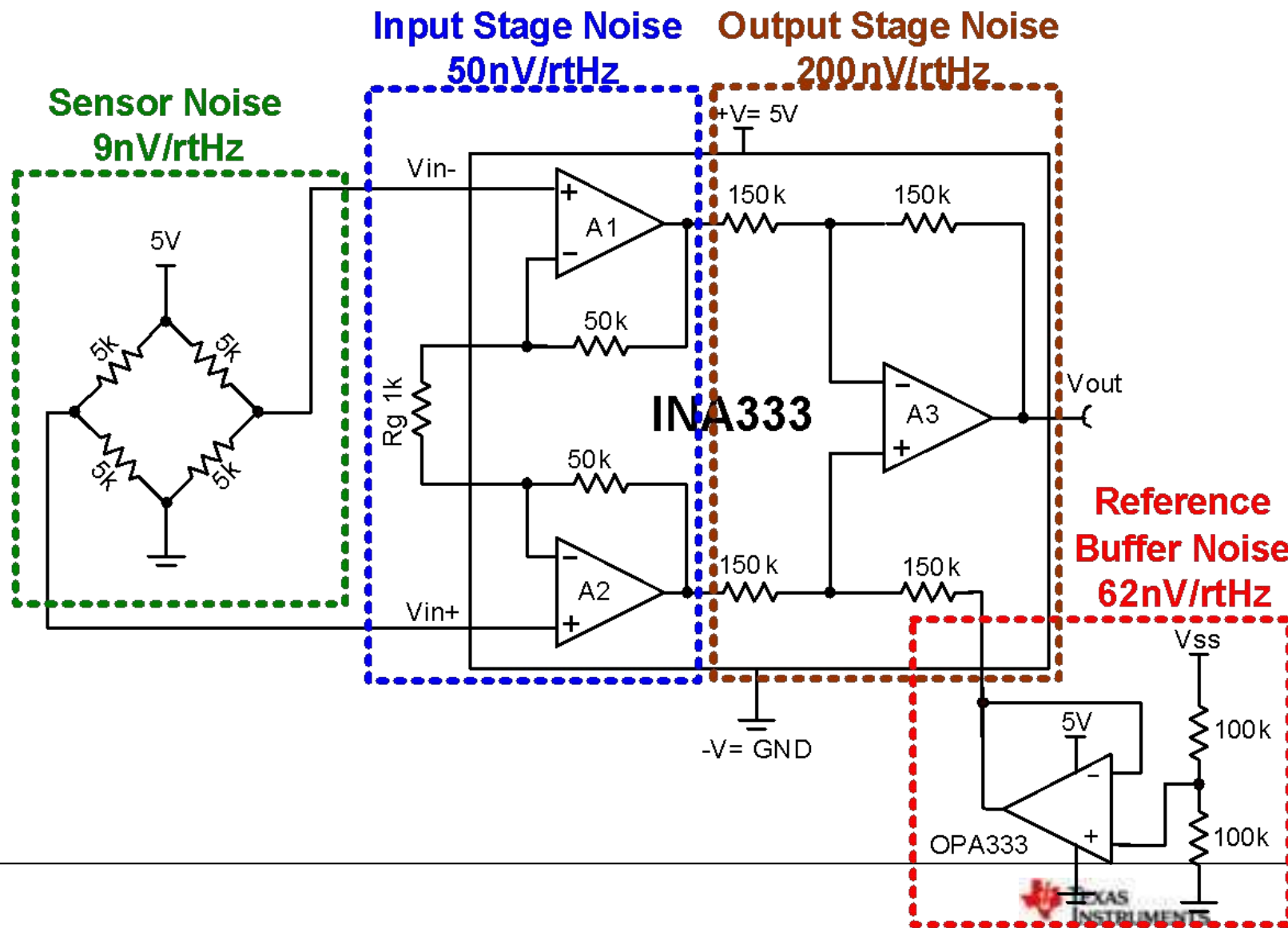
$$i_{nn} \cdot \frac{R}{2} = 0.25 \frac{nV}{\sqrt{Hz}} \quad \text{Voltage noise from current noise}$$

$$e_{in_i} = \sqrt{2(0.25)^2 + 2(6.4)^2} = 9.1 \frac{nV}{\sqrt{Hz}} \quad \text{Total Noise from input resistors and current source}$$



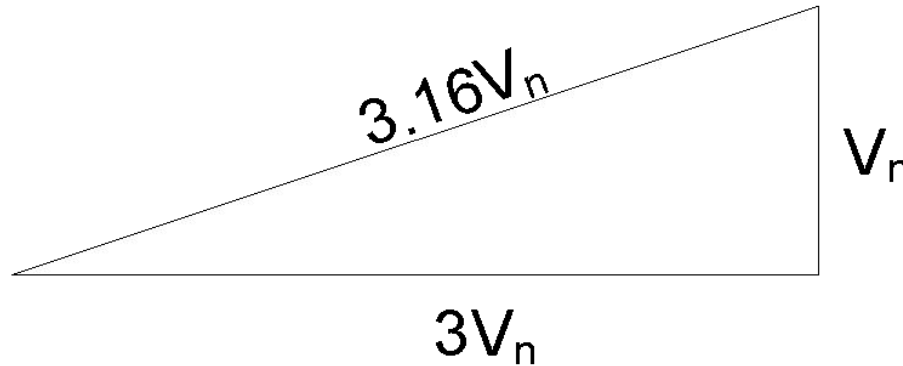


Combine all the noise sources





Rule of 3x



$$\sqrt{\underbrace{(3 \cdot V_n)^2}_{\text{Dominant}} + \underbrace{V_n^2}_{\text{Neglect}}} = \sqrt{9 \cdot V_n^2 + V_n^2} = 3.16V_n$$

When adding two uncorrelated noise terms , the larger term will dominate if it is 3 times larger than the smaller term . You can neglect the smaller term with a relatively small error (i.e. 6%).



For this example compute noise spectral density referred to the input

$$\text{Noise_Spec_Den_RTI} = \sqrt{V_{n_in_stage}^2 + V_{n_bridge}^2 + \left(\frac{V_{n_out_stage}}{G}\right)^2 + \left(\frac{V_{n_ref_buf}}{G}\right)^2}$$

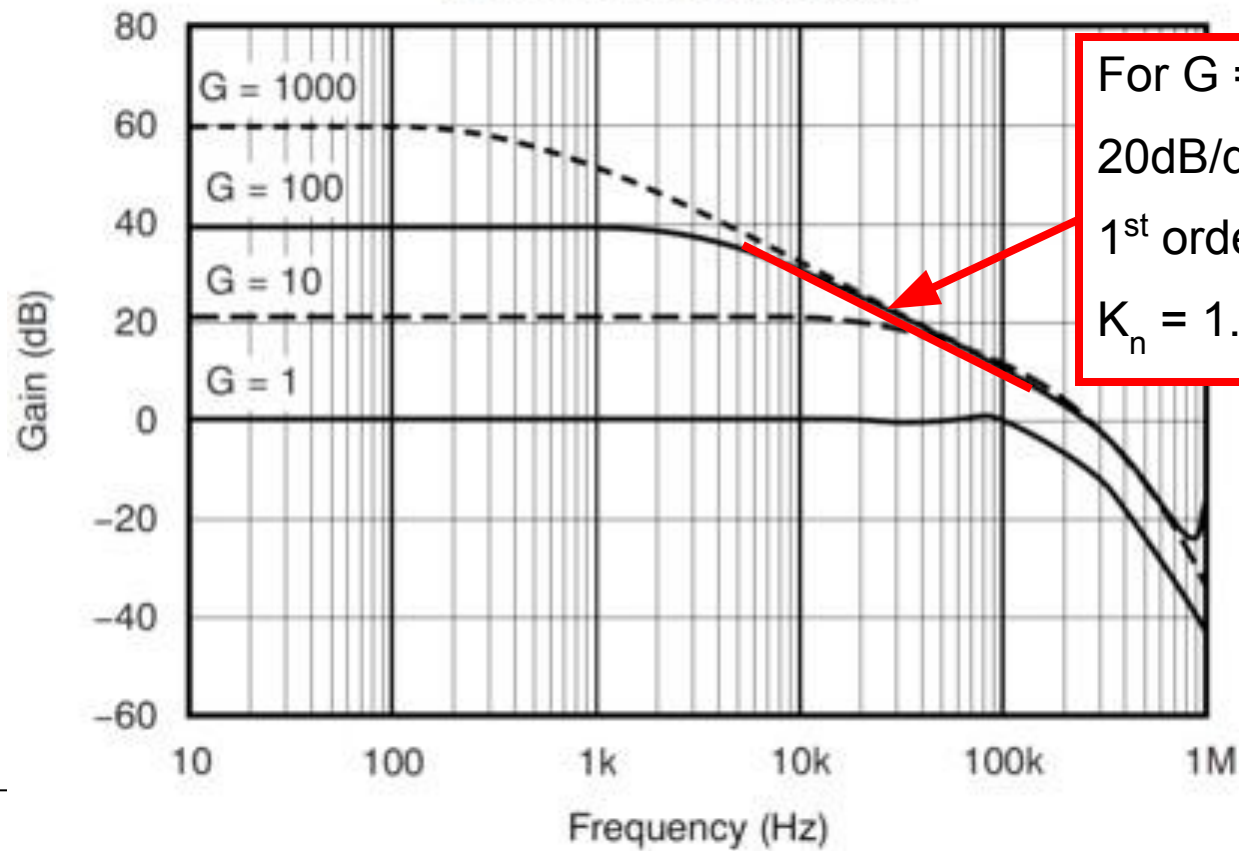
$$\text{Noise_Spec_Den_RTI} = \sqrt{\underbrace{(50)^2}_{\text{Dominant}} + \underbrace{(9)^2 + \left(\frac{200}{100}\right)^2 + \left(\frac{62}{100}\right)^2}_{\text{Neglect}} = \underbrace{50.847}_{\text{Approximately equal to the dominant term}} \frac{\text{nV}}{\sqrt{\text{Hz}}}$$



PARAMETER	INA333			UNIT
	MIN	TYP	MAX	
FREQUENCY RESPONSE				
Bandwidth, -3dB				
G = 1		150		kHz
G = 10		35		kHz
G = 100		3.5		kHz
G = 1000		350		Hz

Bandwidth from Data Sheet

GAIN vs FREQUENCY



For G = 100
20dB/decade
1st order
 $K_n = 1.57$



Calculate RMS Output Noise for INA333 From Voltage Noise

$$G = 100$$

$$V_{in_RTI} = 50.85\text{nV}/\text{rtHz} \quad \text{From "Input referred noise" equation}$$

$$f_H = 3.5\text{kHz} \quad \text{From data sheet table for gain} = 100$$

$$K_n = 1.57 \quad \begin{array}{l} \text{For first order function} \\ \text{See Gain vs Frequency in the data sheet} \end{array}$$

$$BW_n = f_H \cdot K_n = 5.495\text{kHz} \quad \text{Noise Bandwidth}$$

$$e_{n_out} = G \cdot V_{in_RTI} \sqrt{BW_n} = 376.9\mu\text{V}_{\text{rms}} \quad \text{RMS Output Noise}$$

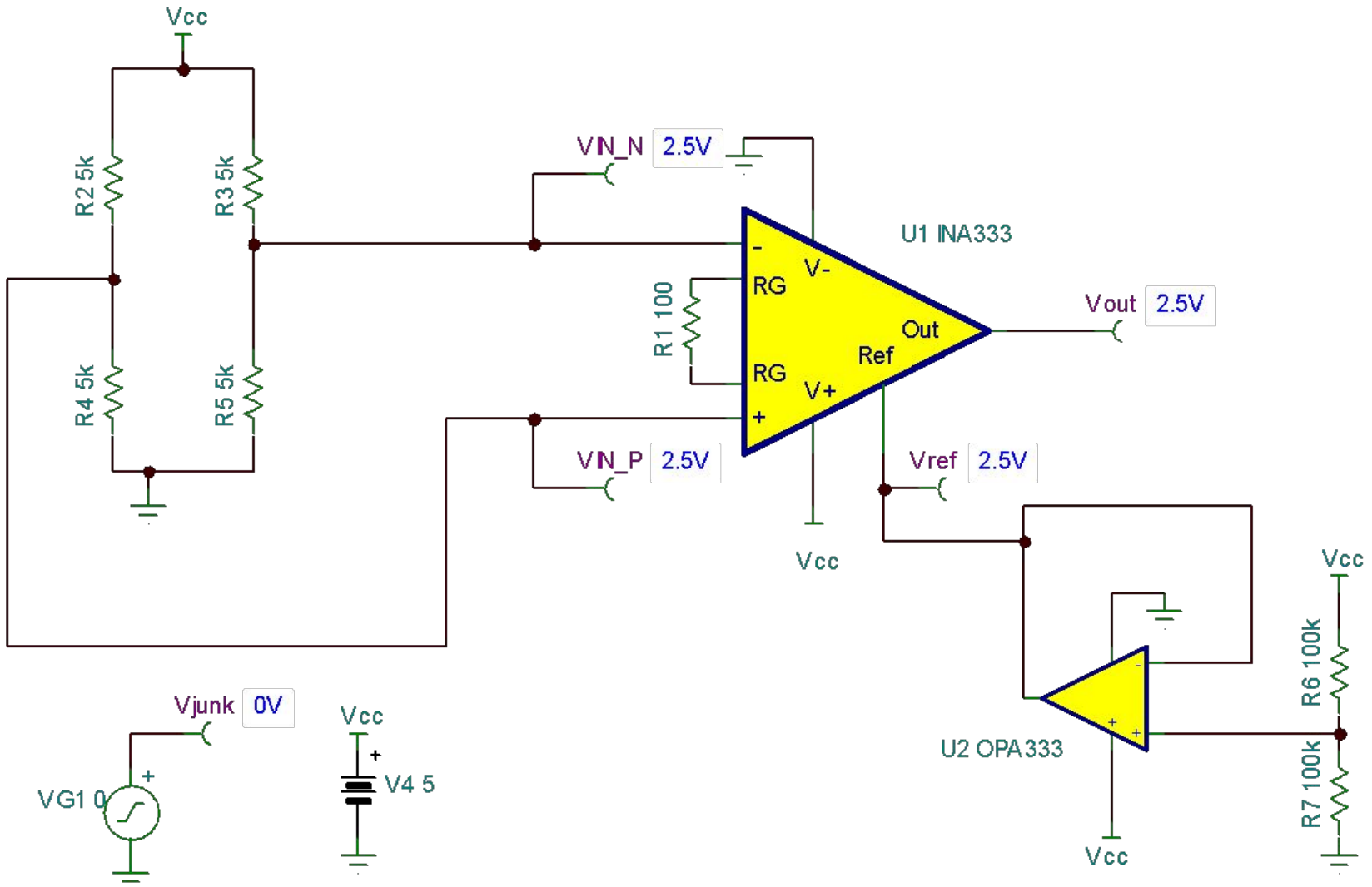
$$e_{n_outPP} = 6 \cdot e_{n_out} = 2.26\text{mV}_{\text{pp}} \quad \text{Peak-to-Peak Output}$$



Simulation of Ramp WA

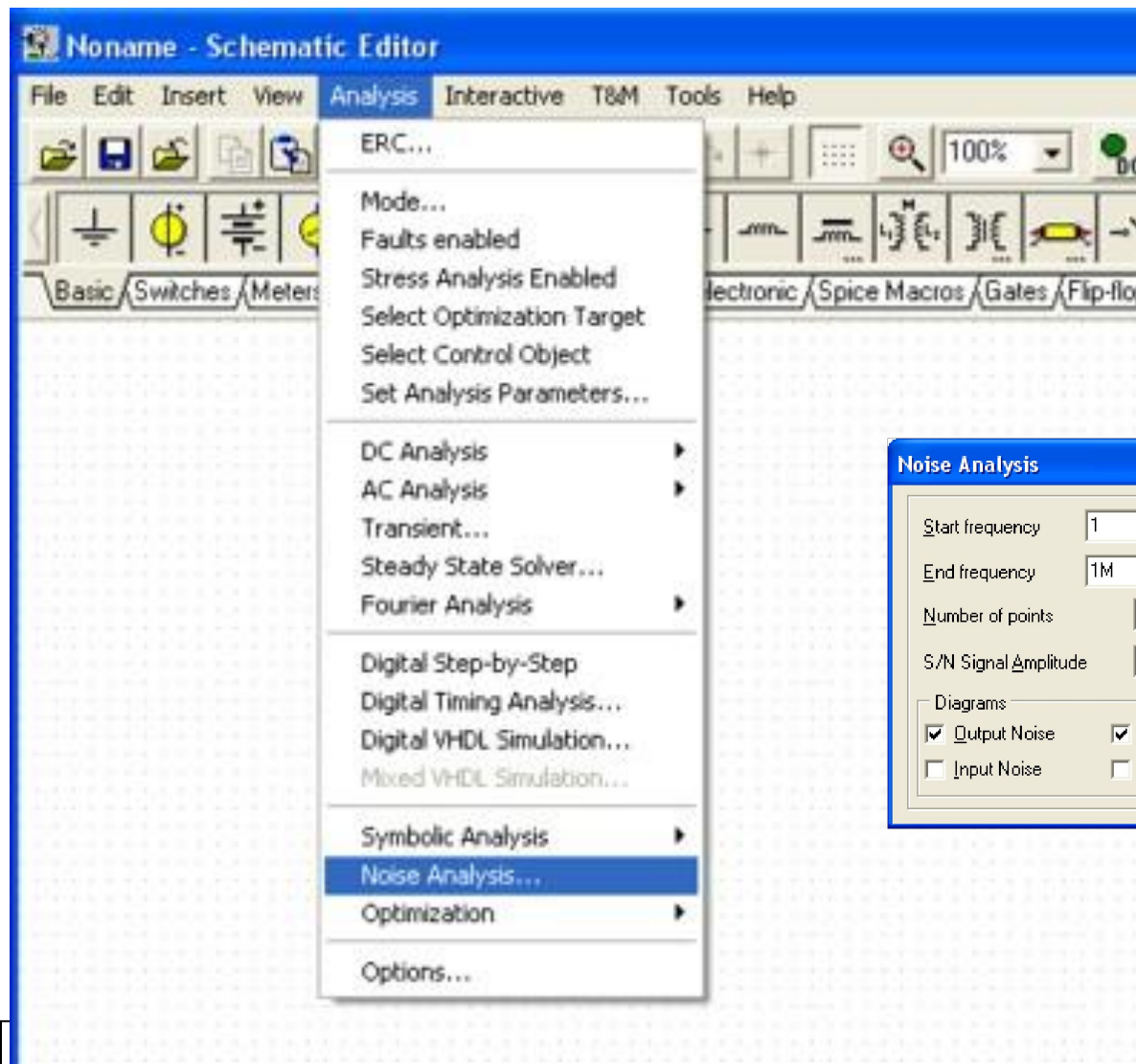


Simulate the Circuit





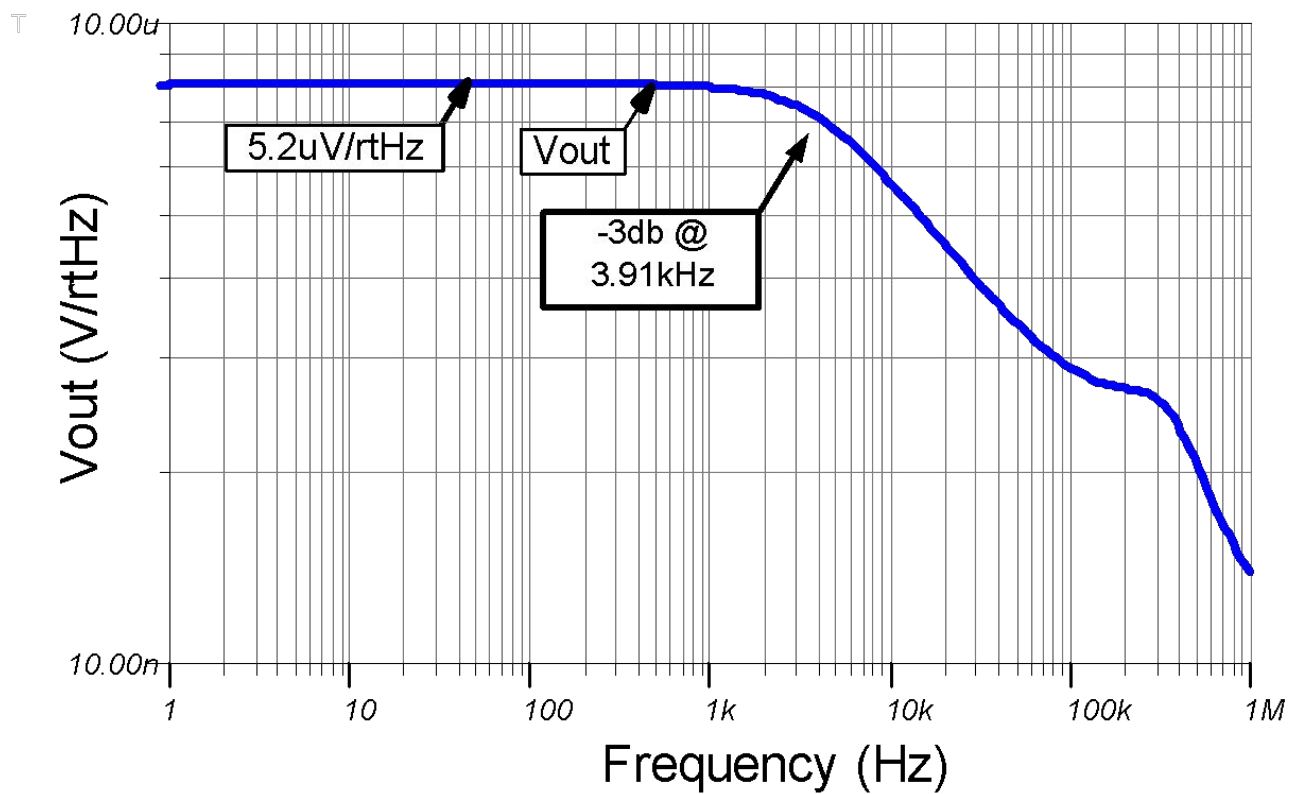
Using Tina Spice





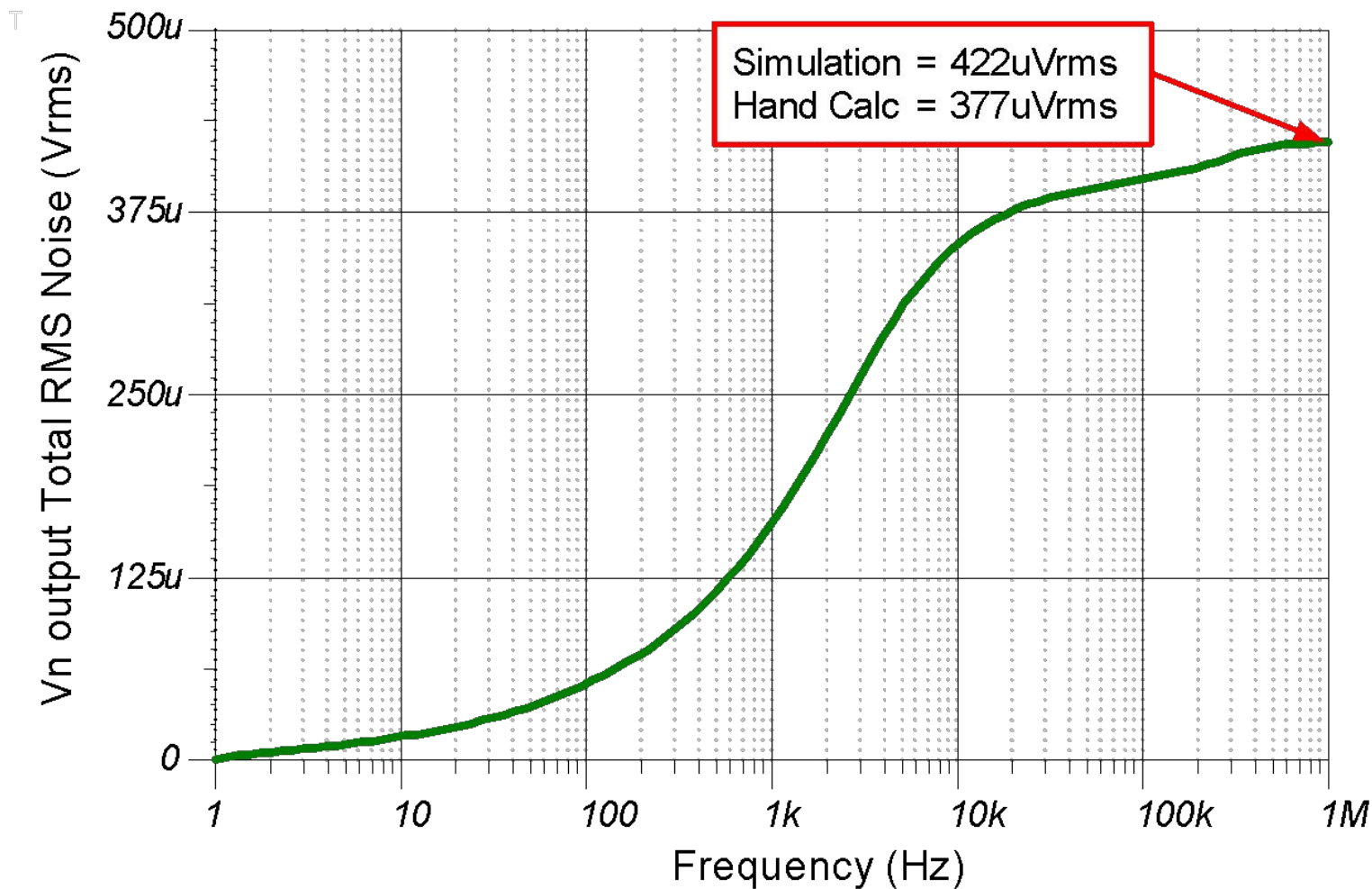
Noise Spectral Density at the Output

Voltage Spectral Density Out vs. Frequency





Total RMS Noise at the Output



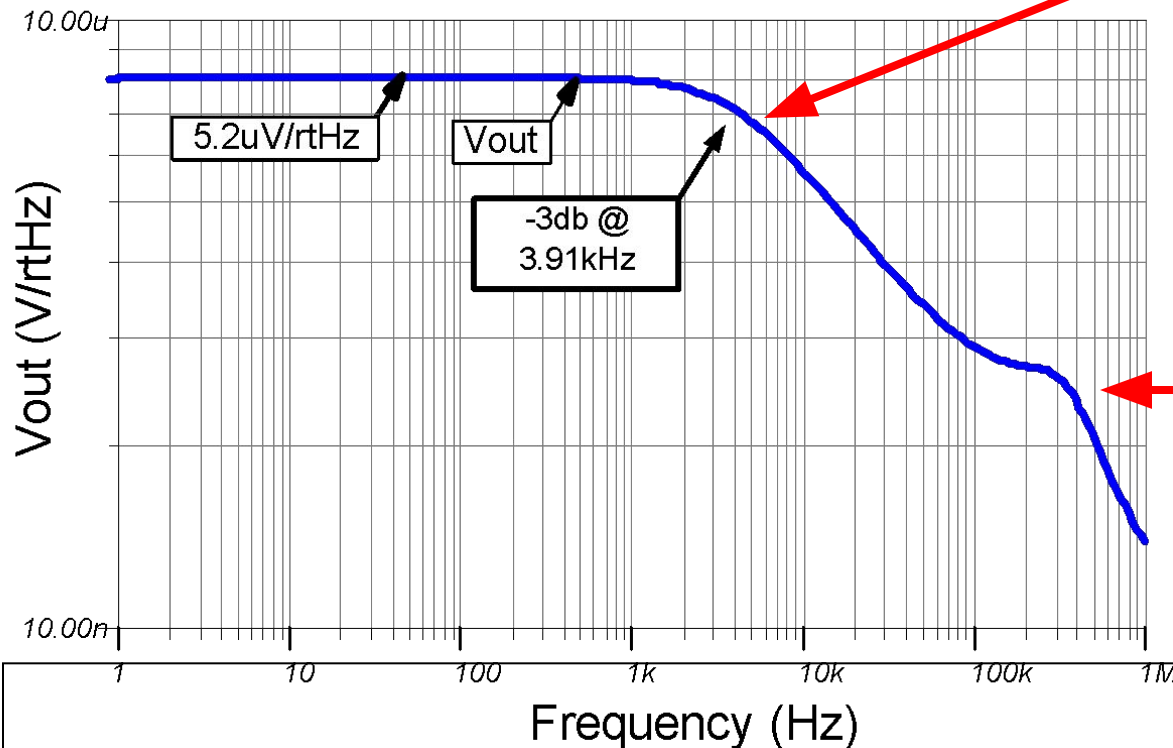


Why doesn't calculation match simulation exactly?

PARAMETER	INA333			UNIT
	MIN	TYP	MAX	
FREQUENCY RESPONSE				
Bandwidth, -3dB				
G = 1		150		kHz
G = 10		35		kHz
G = 100		3.5		kHz
G = 1000		350		Hz

Bandwidth from Data Sheet and simulated bandwidth is different.

Voltage Spectral Density Out vs. Frequency



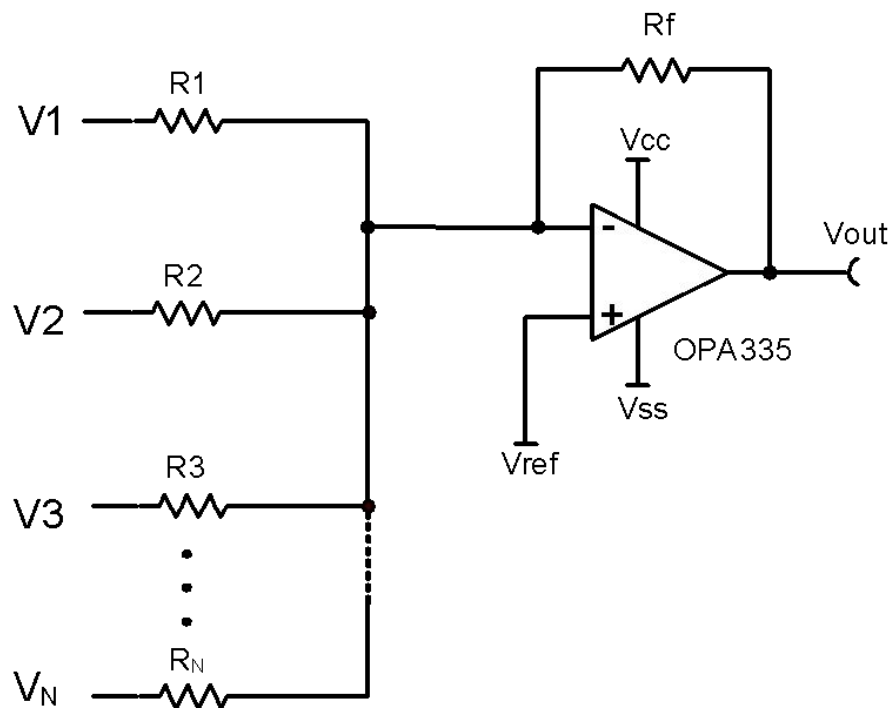
The roll-off was approximated as first order in the calculations. Simulation shows that it is not first order.



REGISTRATION HAS BEGUN



Averaging Circuit



$$V_{out} = V_{ref} - R_f \left(\frac{V_1}{R_1} + \frac{V_2}{R_2} + \frac{V_3}{R_3} + \dots + \frac{V_N}{R_N} \right) \quad [15]$$

For an averaging circuit choose

$$R_1 = R_2 = R_3 = \dots R_N = R$$

$$R_f = R / N$$

$$V_{out} = V_{ref} - \frac{(V_1 + V_2 + V_3 + \dots + V_N)}{N} \quad [16]$$



Noise in Averaging Circuit

$$v_{\text{noise_output}} = \sqrt{\left(\frac{v_{\text{noise1}}}{N}\right)^2 + \left(\frac{v_{\text{noise2}}}{N}\right)^2 + \left(\frac{v_{\text{noise3}}}{N}\right)^2 + \dots + \left(\frac{v_{\text{noiseN}}}{N}\right)^2}$$

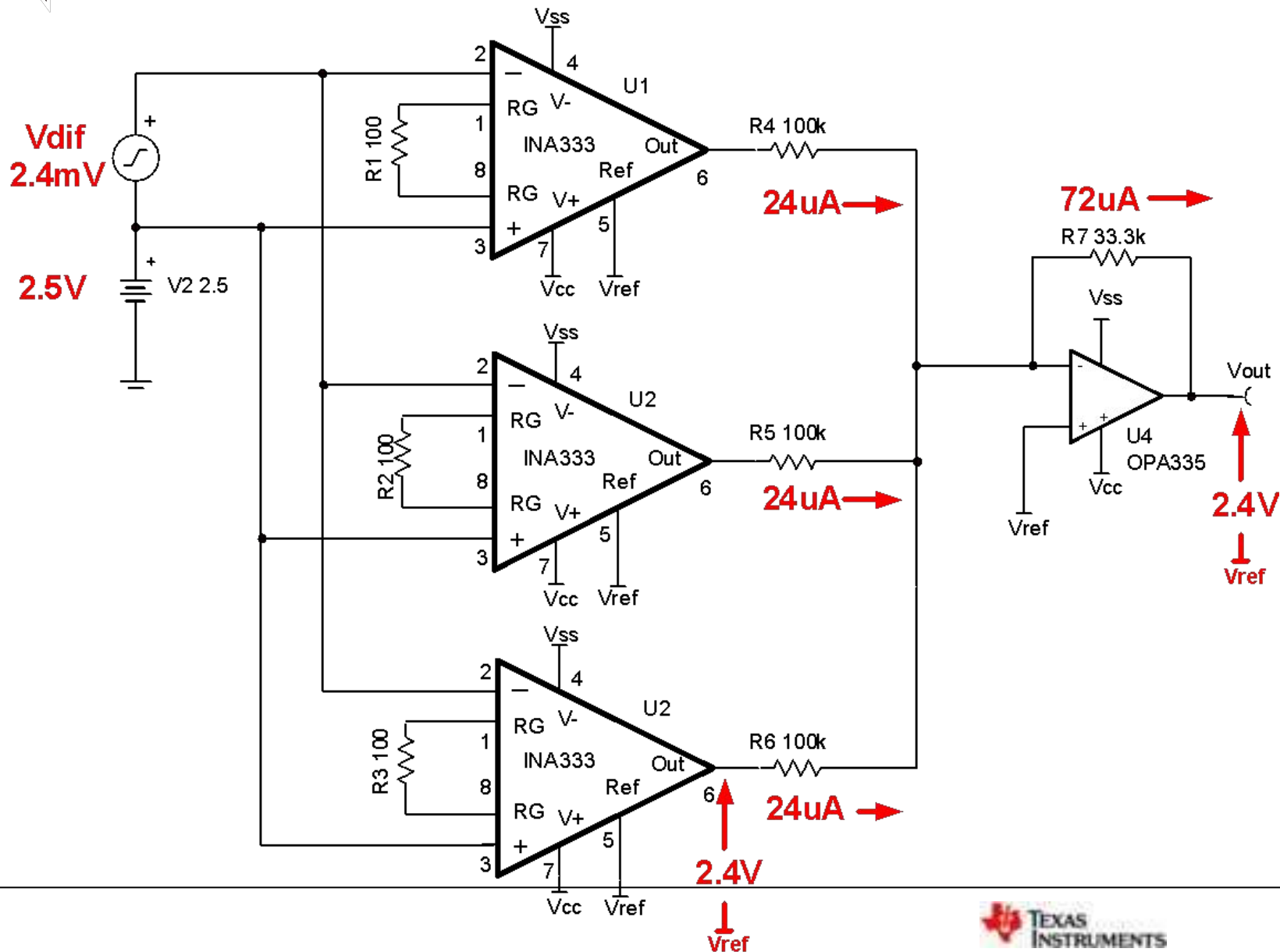
Where v_{noise1} , v_{noise2} , v_{noise3} , ... v_{noiseN} are noise sources

If you assume that v_{noise1} , v_{noise2} , v_{noise3} , ... v_{noiseN} are equal uncorrelated noise sources, then

$$v_{\text{noise_output}} = \sqrt{N \left(\frac{v_{\text{noise}}}{N}\right)^2} = \sqrt{\frac{v_{\text{noise}}^2}{N}} = \frac{v_{\text{noise}}}{\sqrt{N}} \quad [17]$$



Averaging Circuit with INA333

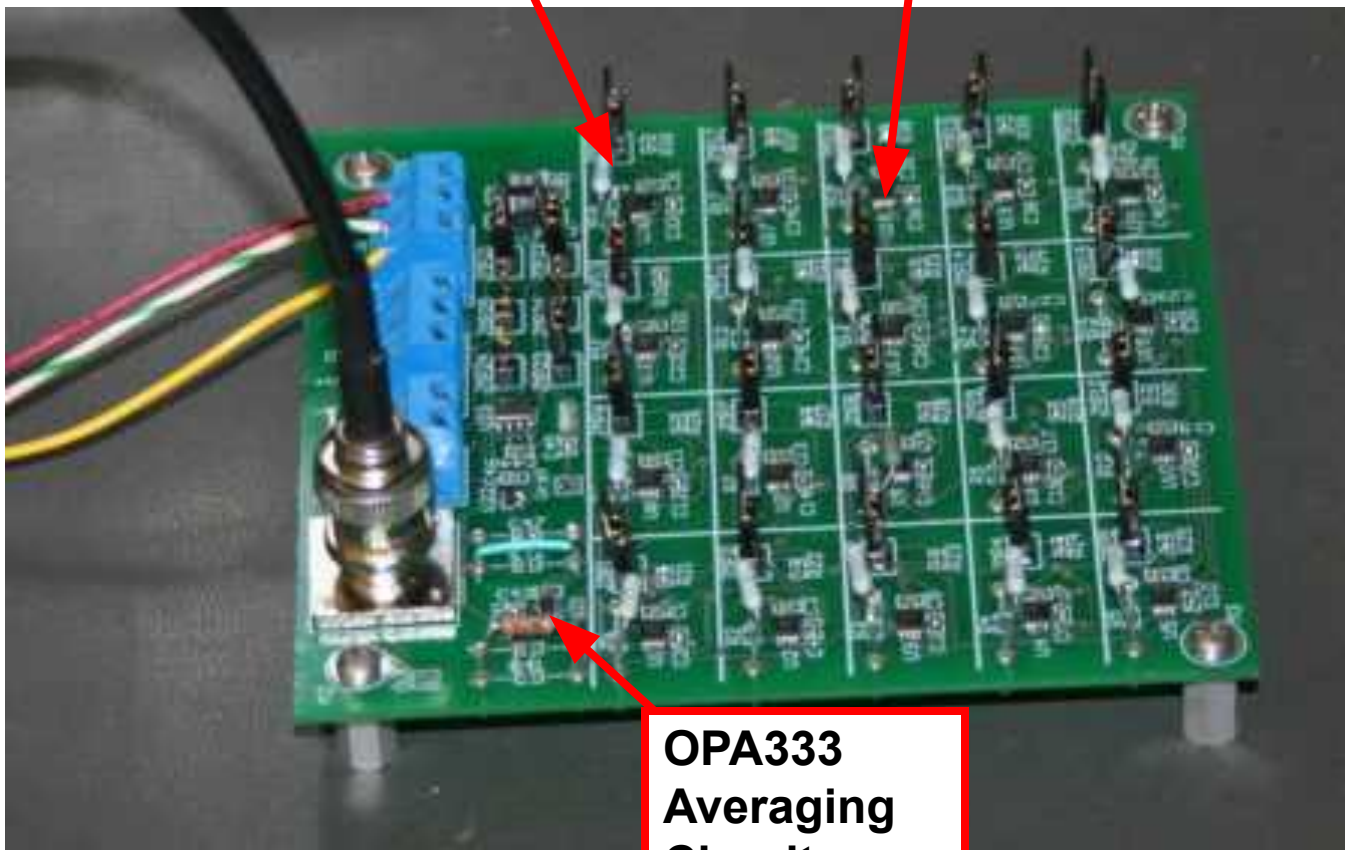




Experiment with 20 Parallel INA333

Socketed Gain Set Resistors

20 INA333 amps in parallel (jumper selectable)



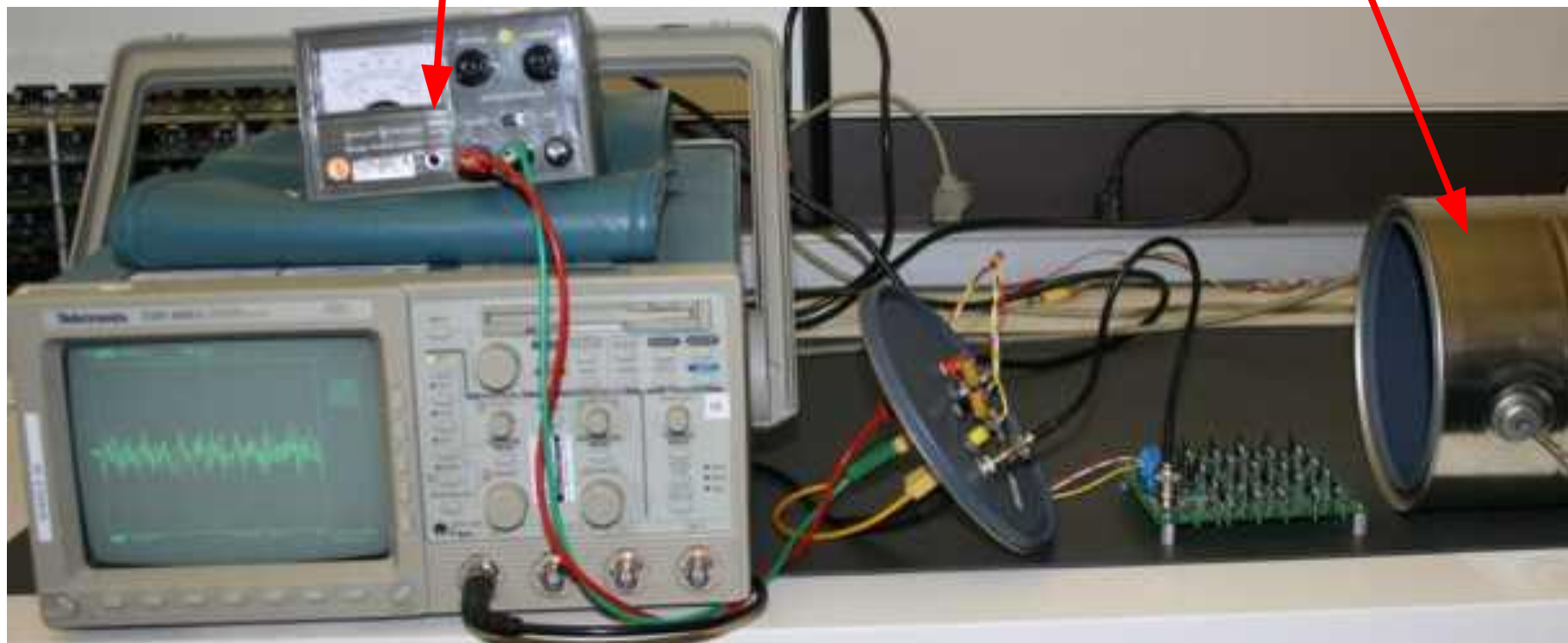
OPA333 Averaging Circuit



Standard Noise Measurement Precautions

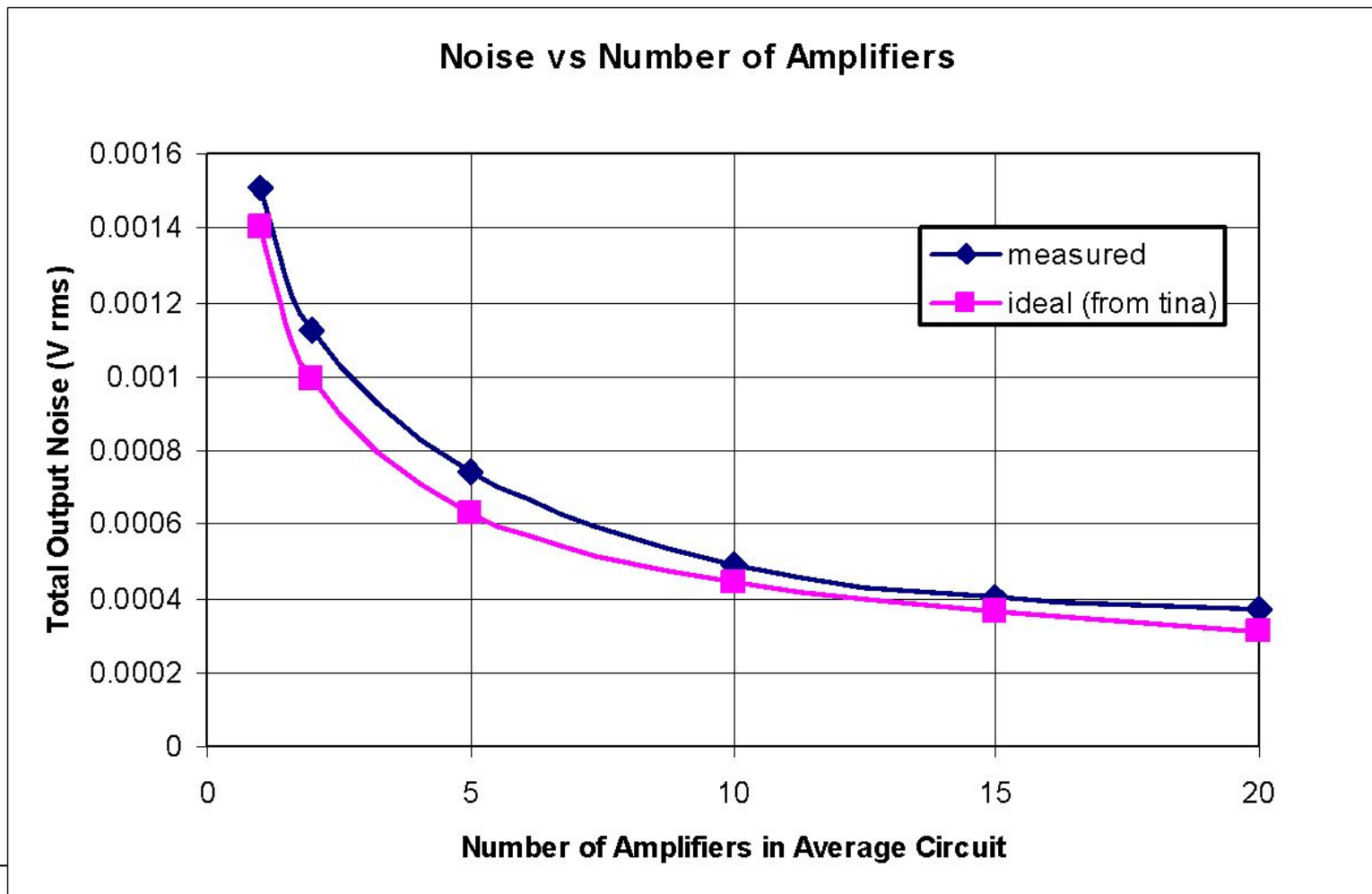
**Linear Power
Source**

**Steel Paint Can
for Shielding**



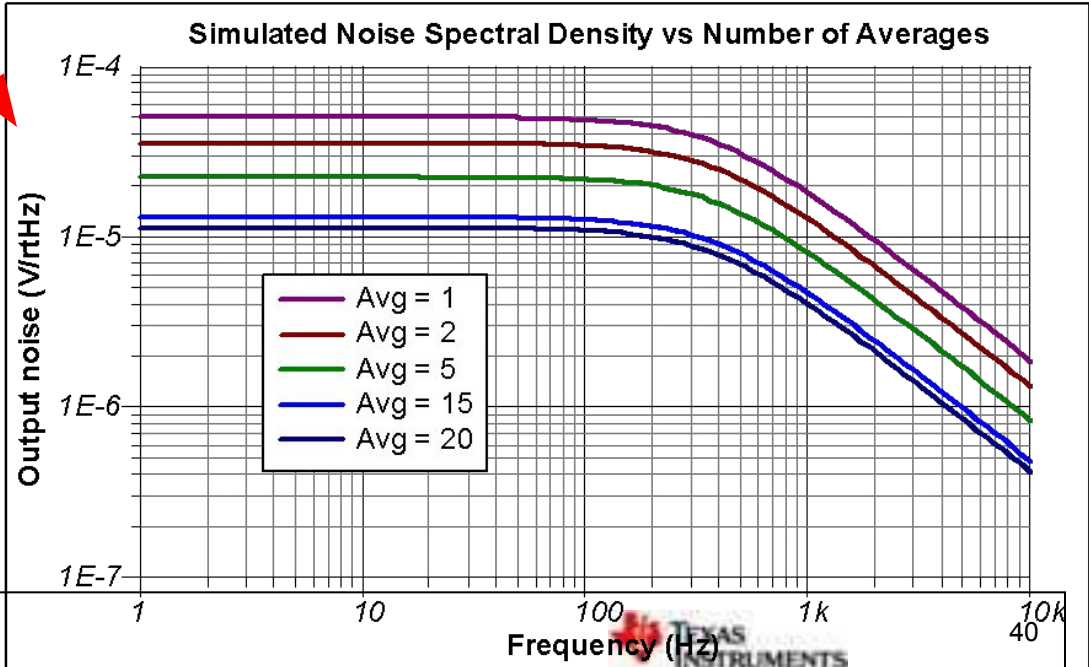
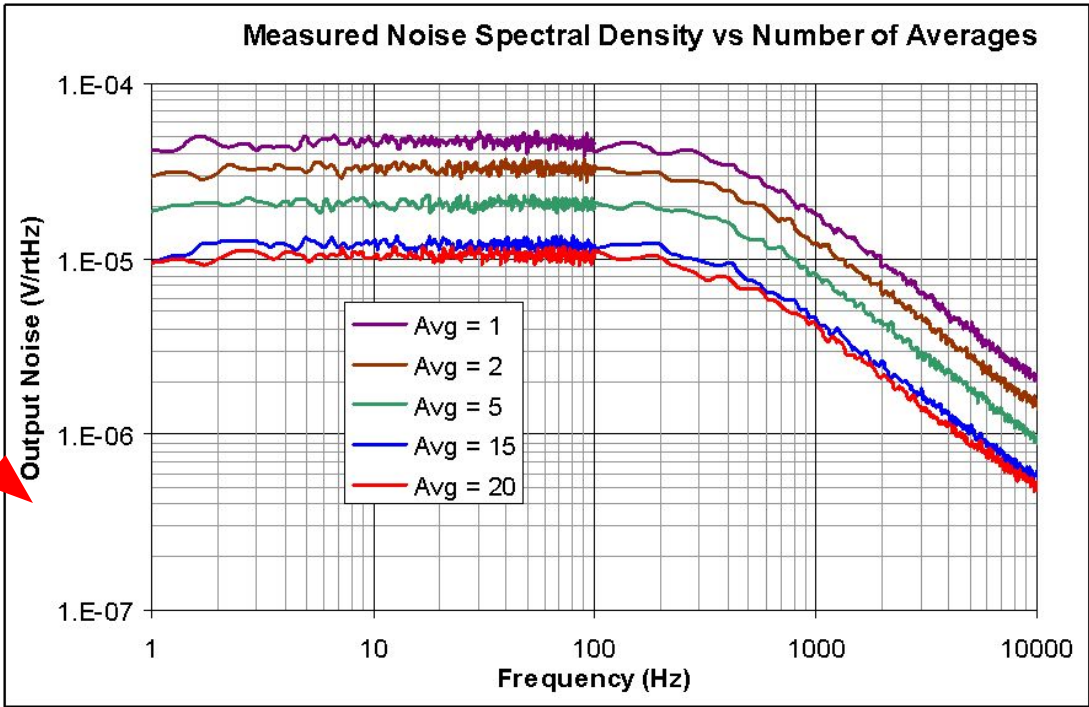


Total Output Noise vs Number of Amplifiers Being Averaged





Measured vs simulated spectral density





References

1. [1] Hann, Gina. "Selecting the right op amp - Electronic Products." Electronic Products Magazine – Component and Technology News. 21 Nov. 2008. Web. 09 Dec. 2009.
<http://www2.electronicproducts.com/Selecting_the_right_op_amp-article-facntexas_nov2008-html.aspx>.
2. Henry W. Ott, Noise Reduction Techniques in Electronics Systems, John Wiley and Sons

Acknowledgments:

1. R. Burt, Technique for Computing Noise based on Data Sheet Curves, General Noise Information
2. T. Green, General Information
3. B. Trump, General Information
8. Matt Hann, General INA information and review

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INA Noise – Calculation and Measurement***